1	Air-sea gas transfer in a shallow, flowing and coastal environment
2	estimated by dissolved inorganic carbon and dissolved oxygen analyses
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1 ABSTRACT

2	We estimated gas exchange rates in Kabira Reef at Ishigaki Island, southwest
3	Japan, using mass balance calculation with dual "biological" tracers; dissolved
4	inorganic carbon (DIC) and dissolved oxygen (DO). With the results during nighttime,
5	we could obtain reasonable gas transfer velocity $k_{\rm w}$ values, all of which exceeded those
6	obtained in wind-dominant studies. The difference is likely due to the contribution of
7	turbulence generated by the interaction of the current and bottom topography. The
8	obtained k_w during high tides is consistent with that by Raymond and Cole (2001),
9	whereas k_w during low tides shows higher, which seems to be caused by enhanced
10	friction with the bottom of the reef or bubble-induced gas transfer by wave breaking at
11	the reef crest.
12	Keywords. Coral reef; gas transfer velocity; dissolved inorganic carbon; dissolved
13	oxygen
14	
15	Introduction
16	The primary controls on the air-water transfer of oxygen or other low-solubility
17	gases in coastal waters are the current, bottom topography and wind stress. Wind stress
18	the instant of the second s
	dominates turbulence in the surface aqueous boundary layer of all systems with depths
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 19 20 21 22 23 	dominates turbulence in the surface aqueous boundary layer of all systems with depths greater than 10 m or wind speeds greater than 8 m s ⁻¹ (Raymond and Cole 2001). Considerable efforts have gone into determining empirical relationships (Liss and Merlivat 1986; Wanninkhof 1992; Wanninkhof and McGillis 1999; Nightingale et al. 2000). On the other hand in shallower, flowing circumstances, even surface turbulence can be dominated by the interaction of the current with bottom topography, and both

1 Physical controls on gas transfer in shallow, flowing coral reef platforms fall

somewhere between these two extremes, and both wind and hydrologically induced
turbulence can be important, depending in part on the depth and width of the system and
in part on the velocity of tidal or river flows (Marino and Howarth 1993).

5 Several methods are used to determine air-water gas transfer velocity in natural 6 water systems. Purposeful gas tracer techniques (e.g., SF₆), which provide the least 7 equivocal answer, are the most promising for natural water studies. Clark et al. (1994) 8 applied this method (SF₆ and 3 He) to unidirectional water flow system like the Hudson 9 River. This approach was rarely used to more complex flow systems like estuaries, coral 10 reefs. Many experiments to determine gas exchange rates in coastal environments have 11 been conducted using the "helmet" method (Clark et al. 1994), in which the gas 12 exchange rate is calculated from the rate of gas accumulation into an inverted dome 13 floating on the water surface. The major problem is the degree to which the floating 14 dome disturbs the surface turbulence regime; the physical driving force behind the gas 15 exchange is unknown. Laboratory experiments have found little agreement between gas 16 exchange rates determined by the helmet method and other approaches (Clark et al. 17 1994). Recently, Tokoro et al. (2007, 2008) examined and evaluated this method by 18 comparing the energy dissipation rates measured inside and outside the floating 19 chamber and confirmed that there was no significant disturbance to the surface 20 turbulence regime. Aqueous turbulence analysis (micrometeorological technique) is also 21 being common method to determine gas transfer velocity in the coastal waters. Zappa et 22 al. (2003, 2007) combined various techniques to measure surface turbulence (surface 23 renewal rates, turbulent scales, and energy dissipation rates).

24

Mass balance calculation is an alternative method (e.g. Marino and Howarth
 1993; Cai et al. 1999), however, the magnitude and variability of the sources and sinks
 of the dissolved gas must be well known (Marino and Howarth 1993; Raymond and
 Cole 2001).

In this study, we estimated gas transfer velocities in the shallow, flowing and coastal environment of a coral reef platform using mass balance calculation with dual "biological" tracers; dissolved inorganic carbon (DIC) and dissolved oxygen (DO). Few studies have used these tracers to determine gas transfer velocity; however, recent progress in analytical methods measuring DIC and the relative simplicity of our field situation made their use practicable.

11 Because of their high metabolic activities, coral reefs generally have wide diel 12 variations in DIC and DO. With regard to CO₂, metabolic fluxes (photosynthesis or 13 respiration) significantly dominate over gas exchange flux (e.g. Frankignoulle et al. 14 1996). Thus, we postulated that the diel variation of DIC is determined solely by 15 metabolic activity in a limited water residence time. On the other hand, DO gas 16 exchange flux is usually comparable to that of metabolic fluxes. Based on the differing 17 characteristics of these gases in coral reefs, we define DIC as a "biologically reactive 18 but physically conservative" tracer and DO as a tracer "both biologically and physically 19 reactive." Thus, the gas transfer velocity of O_2 can be calculated by eliminating the 20 estimated metabolic contribution of DIC variations. 21 Several investigations were conducted to measure DO and DIC simultaneously, 22 mainly for open ocean environments. In the open ocean settings, DIC does not act as

23 physically conservative tracer due to the relatively low metabolic rates. Moreover, the

24 difference of inventory between DO and DIC in the mixed layer yields the difference of

1	equilibration time with respect to gas exchange (e.g., Nakayama et al. 2000; McNeil et
2	al. 2006). Recently, Körtzinger et al. (2008) demonstrated long-term (1-year)
3	observational results for DO and pCO2 at the central Labrador Sea and obtained a
4	consistent gas transfer velocity with previous studies (Wanninkhof 1992; Wanninkhof
5	and McGillis 1999) at wind speed more than 10 m s ⁻¹ , with selected observation period.
6	A mass balance calculation with biological tracers includes several
7	uncertainties. First, the coral reef ecosystem is generally dominated by calcifying
8	organisms as corals and calcifying algae. Although calcification decreases DIC, DO
9	does not change. Therefore, calcification rates must be determined. They can be
10	calculated by temporal or spatial changes of seawater total alkalinity (TA). Second, the
11	ratios of DO change to DIC change during photosynthesis and organic matter
12	decomposition/respiration must be defined by a photosynthetic quotient (PQ) and
13	respiratory quotient (RQ), respectively. Third, the sites of metabolism that play roles in
14	the tracer sources must be determined. Finally, if water advection and mixing processes
15	are complicated, the determination of water fluxes is very difficult.
16	Kabira Reef at Ishigaki Island, southwest Japan, is an ideal location to
17	minimize these uncertainties. The current analysis of Yamano et al. (1998) showed that
18	the circulation pattern under calm or northern wind conditions is characterized simply
19	by an inflow of offshore waters into the moat over the reef crest and an outflow through
20	a prominent channel. Because most organisms are concentrated around the reef crest,
21	the metabolism site can be easily described.
22	

23 MATERIALS AND METHODS

24 Study site

1	Kabira Reef is a well-developed fringing reef located on the north coast of
2	western Ishigaki Island, southwest Japan (Figs. 1, 2). Ishigaki Island is situated in a
3	monsoon area, where the dominant wind direction is from the south in summer and
4	north in winter. Yamano et al. (1998) concluded that wind direction markedly
5	influences the seasonal patterns of water circulation at Kabira Reef. Under calm or
6	northern wind conditions, the circulation pattern is characterized by an inflow of
7	offshore waters into the moat over the reef crest and an outflow through a prominent
8	channel, whereas southern wind conditions this pattern is weakened or disturbed
9	(Yamano et al., 1998). Thus, during northern to northeastern winds, metabolic activities
10	with respect to primary production can be observed over the entire reef, if waters from
11	offshore and the channel are taken as the initial and final values, respectively. Figure 2
12	shows that the trajectories of input water to Kabira Reef during the observation periods
13	clearly reproduce the flow pattern described above.
14	Research methods
15	Observations were conducted on 7-8 March 2003. To calculate water
16	mass balance, electromagnetic current meters (ACM-8M, 16M, Alec Electronics) were
17	situated at three points and set to measure every 5 minutes (Fig. 2). The sensor-heads
18	were set 50 cm above the bottom. At the point M800 (24°28'22.8"N, 124°8'42.5"E),
19	the volume transport of water entering from offshore was measured; that of water
20	exiting through the channel was measured at the point E350 (24°27'56.5"N,
21	124°8'47.4"E). The other current meter, at the point W400 (24°28'26.9"N,
22	124°8'17.0"E), was situated to confirm whether there was additional flow from or to
23	northwest (parallel to the shoreline) or not. As a result, we did not observe significant
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1	used afterward. We also conducted drifting buoy experiments that were described by
2	Miyajima et al. (2007) in order to determine the length of water path and its residence
3	time in the reef. A small drogue made of a floating buoy and an underwater cross-shape
4	plate was released near the point M800, and it was followed by the boat to determine its
5	position using GPS. Nine experiments were conducted randomly during the observation
6	period. Tracks of the drifting buoy were plotted in Fig. 2. Oceanographic and
7	meteorological parameters were observed at E350. Water temperature, salinity, tidal
8	level, and dissolved oxygen were monitored every 5 minutes by DO-CTD sensor
9	(Hydrolab DATASONDE 4 α). Salinities were calibrated by Portasal TM salinometer
10	(Guildline Instruments) with IAPSO seawater standards and bottled seawater samples
11	that were collected irregularly. The O_2 probe with membrane electrode was calibrated
12	prior to deployment using oxygen-free (0 $\%$ in saturation) and oxygen-saturated (100 $\%$
13	in saturation) solutions. These solutions were measured independently by conventional
14	Winkler titration. Sensor drift was also corrected every day by measuring saturated
15	solution. Seawater samples for DIC and TA analysis were collected every 2-hour until
16	0800 March 7 and 1-hour afterward in 500-ml glass bottles (DURAN®) from surface
17	water at E350 and then poisoned using HgCl ₂ solution. Samples from offshore were
18	taken once a day with a same manner. DIC and TA were determined by continuous-
19	flow through a DIC and TA analyzer developed by University of Tokyo, Japan Science
20	and Technology Agency, and Kimoto Electronics (Kimoto et al. 2001; Watanabe et al.
21	2004; Watanabe 2004). For DIC, the sample water was acidified with phosphoric acid,
22	and the extracted CO ₂ was measured using a non-dispersive infrared gas analyzer (LI-
23	6252, LICOR). For TA, the sample water and a specific proportionate HCl solution
24	were mixed, and the pH difference between the initial and acidified water was measured

1	using a combined glass electrode. The precisions of the water temperature, salinity, DO,	
2	DIC and TA were 0.1 °C, 0.05 psu, 1.5, 2 and 1.5 $\mu mol~kg^{\text{-1}}$, respectively (1 S.D.). The	
3	accuracies of the DO, DIC and TA were 3, 3 and 4 $\mu mol~kg^{\text{-1}}$, respectively. Those of the	
4	water temperature and salinity were not evaluated in this study.	
5	DIC and TA were normalized to the salinity of 35 conventionally like,	
6		
7	$NDIC = DIC^{0}35/S $ (eq.1)	
8		
9	where TA is treated similarly as NTA.	
10	Wind, air temperature, solar radiation, humidity, and air pressure were monitored every 5	
11	minutes by an Aanderaa® weather station situated at E350 with the height of 5 m above	
12	mean sea level. Horizontal wind speeds were converted to those at 10 m height by	
13	following equations (Brutsaert, 1982).	
14		
15	$U_{10}(ms^{-1}) = u_k^* \ln \frac{0}{z_0}$, $u_* = C_{d0.5} u_{obs}$ (eq.2)	
16		
17	where U_{10} , u*, k, z ₀ , C _d and u _{obs} represent wind speed at 10 m height, friction velocity,	
18	von Karman constant (0.4), roughness at water surface, drag coefficient and observed	
19	wind speed at 5 m height (ms ⁻¹), respectively. Surface roughness was calculated as $z_0 =$	
20	$1.65 \times 10^{-4}u_{*1.4}$, and drag coefficient of 1.15×10^{-3} was applied according to the study by	
21	Emmanuel (1975).	
22		

1 OBSERVATIONAL RESULTS

Figure 3 shows a time series of meteorological and oceanographic observations 2 at Kabira Reef on 7-8 March 2003. The average wind speed (Fig. 3a) was 8 m s⁻¹ at 5 m 3 4 above sea level with the dominant direction N to NNE, and the wind-driven surface 5 flow from offshore was assumed to be constantly northern. From 1100 to 1400 on 6 6 March, 20 mm rainfall resulted in relatively low salinity at the beginning of the 7 observation period (Fig. 3b), after which salinity gradually increased. Salinity was 8 almost constant throughout the observation period with tiny diel variation associated 9 with tidal changes. Offshore salinities were constant at 34.97. The average tidal 10 difference of 1.2 m corresponded to the middle tide toward neap (Fig. 3c). The average 11 current direction at M800 (reef crest) was almost the same as the N to NE wind 12 direction (Fig. 3d) and offshore water inflow over the reef crest was almost parallel to 13 the wind direction. The direction of water exiting via the southeast channel was nearly 14 perpendicular to the channel, and was constant throughout the observation period (Fig. 15 3e). Dissolved oxygen was almost less than saturation during the observation period, 16 except on 8 March (Fig. 3f), when the daytime concentration exceeded saturation level 17 due to the increase of net productivity associated with solar radiation. DIC and DO 18 variations were nearly symmetrical (Fig. 3g). TA was low during the daytime and close 19 to offshore values at night (Fig. 3h). Offshore DO, NDIC and NTA were almost constant through the observation period, namely 198, 2019 and 2334 µmol kg⁻¹ for 0900 20 March 7 and 204, 2019 and 2339 µmol kg⁻¹ for 0840 March 8, respectively. Additional 21 22 offshore samples were taken for DIC and TA at 1830 March 6, and there was no 23 significant difference from other two results as 2017 and 2335 µmol kg⁻¹ for NDIC and 24 NTA, respectively.

2	ESTIMATION OF GAS TRANSFER VELOCITY kw DERIVED
3	FROM DO-DIC ANALYSES
4	Determining gas transfer velocity was a two-step process involving the
5	calculation of 1) the residence time of reef water and 2) the metabolic rates (production
6	and respiration rates) of reef organisms.
7	
8	Calculation of the residence time of reef water
9	The residence time of reef water was calculated as a long section of the water
10	path divided by the line flux of the water:
11	
12	$T = (L \times D_{avg}) / (S_i \times D) \times f $ (eq.3)
13	
14	where L, $D_{\text{avg}},S_{\text{i}},\text{and}D$ represent the length of the path from the reef edge to the
15	channel, spatial average water depth along the pass, current speed, and water depth at
16	the reef edge, respectively. The L value of 1100 m was based on water trajectory results
17	obtained from buoy experiments. D_{avg} was estimated from trajectories and topographic
18	sections of Kabira Reef. S_i and D were derived from observed values at E350. The term
19	f is a correction factor that represents the ratio of mean water flux at the reef exit to the
20	water flux observed at E350. This factor was determined by comparison with the actual
21	residence time observed in the drifting buoy experiments. Figure 4 indicates both the
22	observed and estimated residence times, indicated by the filled diamonds and solid line,
23	respectively. Based on the three observations, we determined an f value of 0.7, which
24	implies that the water flux at E350 was 1.4 times greater than average. This factor

1	appears to be constant throughout the observation period. The calculated residence time
2	was 1.1 h on average, with the maximum observed at 0200 (1.5 h) and the minimum
3	observed at 1000 (0.8 h). The relative error of ± 5.8 % was obtained based on the
4	precisions for depth and current measurements provided by the manufacturer. Residence
5	time tended to be less during flood tides than at ebb tides. In a single tidal cycle,
6	relatively higher values were observed 2 hours before and after the ebb tide.
7	
8	Calculation of the metabolic rates
9	Metabolic rates (net community production; NCP) for the reef community were
10	calculated from changes in TA and DIC between offshore and E350 (eq.4). By
11	definition, calcification decreases TA as 2 moles per mol of CaCO ₃ formation, so that
12	half of the TA changes correspond to the calcification rate for the entire reef.
13	
14	NCP (mmol m ⁻² h ⁻¹)= [(DIC _{final} - DIC _{initial}) - (TA _{final} - TA _{initial})/2] × D _{avg} / T
15	(eq.4)
16	where DIC_{final} and TA_{final} represent the observed NDIC and NTA at E350, respectively,
17	and DIC _{initial} and TA _{initial} represent offshore NDIC and NTA, respectively, using the
18	average values of the two offshore seawater samplings (Fig. 3g and h). This calculation
19	was same as that indicated by Gattuso et al. (1996), except for influence of CO_2 gas
20	exchange on metabolic rates (see discussion in detail). Daytime production on 8 March
21	was higher than that on 7 March due to higher irradiance. Nighttime respiration differed
22	slightly between 7 and 8 March, but was essentially constant each night. The metabolic
23	rates we obtained agree well those obtained by Kayanne et al. (2005) in the same season
24	at Shiraho Reef on the east coast, based on fixed-point observations during slack-water

1 periods.

2	The O ₂ transfer flux between the atmosphere and reef water was determined
3	using the calculated water residence time, metabolic rates and temporal DO
4	concentration observed at E350. To convert carbon production or respiration to those of
5	O ₂ , we used metabolic quotients, such as the photosynthetic quotient (PQ) or respiratory
6	quotient (RQ). Gattuso et al. (1999) obtained a uniform PQ of 1.1, based on two
7	different reef observations, and concluded that this value agreed with previous
8	investigations at other sites. Strickland and Parsons (1978) proposed a RQ value of 1.0
9	for normal marine populations exposed to moderate light intensities. Several studies that
10	estimated coral reef ecosystem RQs (Kinsey 1978; Barnes and Devereux 1984) did not
11	find RQ to differ significantly from unity. Consequently, we used PQ (NCP > 0) and
12	RQ (NCP $<$ 0) values of 1.1 and 1.0, respectively. Anoxic decomposition of organic
13	materials such as sulfate reduction, which influences not on DO but on DIC and TA
14	alone, can be neglected. Since bottom sediments of the reef are composed mostly of
15	coarse bioclastic sands or rubbles (fragments of coral skeletons and foraminiferal tests;
16	Yamano et al. 2000), sedimentary environment can be regarded as oxic.
17	Finally, O ₂ transfer flux was calculated as follows:
18	
19	$G (mmol/m2/h) = (DO_{final} - DO_{initial}) \times D_{avg} / T - M_{O2} $ (eq.5)
20	
21	where M_{02} is 1.1NCP (NCP>0) and 1.0NCP (NCP<0), respectively. We converted the
22	obtained gas exchange flux G to gas transfer velocity $k_{w,O2}$, using the saturation degree
23	of O ₂ .
24	

1

$$k_{w,02} = G / (DO_{avg} - DO_{sat})$$
 (eq.6)

 2
 3
 The DO_{avg} was determined by the average of DO_{mitial} and DO_{finul}, as defined in eq. (5).

 4
 For comparison with previous studies, $k_{w,02}$ was normalized to Schmidt number of 600.

 5
 $k_{w,600} = k_{w,02} (600/Sc_{02})^{-0.5}$
 (eq.7)

 7
 $Sc_{02} = 1953.4 - 128t + 3.9918t^2 - 0.050091t^3$
 (eq.8)

 9
 where t represents water temperature in deg. C. Schmidt number of O₂ was determined

 10
 using a polynomial fitting equation by Wanninkhof (1992).

 11
 Total errors for estimating NCP and k_w were evaluated by summing up of

 12
 relative errors for each component, then obtained as 6.5 % and 9.3 % for NCP and k_w in

 13
 1 S. D., respectively.

 14
 DISCUSSION

 16
 Table 1 lists the estimated k_w values derived from the combined DO-DIC

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 analysis. In general, k_w should have positive values; however, we found negative values

 18
 in daytime, caused by the prescribed PQ value. Obtaining positive values for all periods

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 required a PQ value of 0.5. If this is the case, however, several k_w values of the order of

 19
 hundreds cm h⁻¹ will be found in daytime on 8 March, which are unrealistic numbers.

 20

23 concentrations greater than saturation. Our results may support this and suggest that a

1 constant PQ value is inapplicable. On the other hand, nighttime kw values were 2 relatively stable, implying that a constant RQ value can be applied. Consequently, the 3 following discussion of gas transfer velocity is based on the nighttime kw values obtained on 7 and 8 March. 4 5 Consistent gas transfer velocities obtained for nights of 7 and 8 March were 49 ± 15 and 49 ± 14 cm h⁻¹, respectively. The average horizontal wind speeds were 8.9 on 6 7 March and 8.7 m s⁻¹ on 8 March. All of the results exceeded the estimated wind-7 8 driven transfer velocity by four conventional algorithms (Fig. 5), clearly demonstrating 9 the occurrence of surface turbulence created by the friction of water passing over the 10 bottom of the reef. We divided the results into periods of higher and lower tidal levels, 11 based on the average water depth of the trajectory (1.26 m). Except for an outlying 12 result at 0000 7 March (upper-left in Fig. 5), the average values for high and low tides were 43œ8 and 52œ15 cm h⁻¹, respectively. The lower water depth tended to result in 13 14 greater gas transfer, although the average horizontal wind speed was slightly lower during the period (8.7 at low tide and 9.0 m s⁻¹ at high tide; Fig. 5). 15 16 As seen in Figure 5, the average value during high tides (filled square) falls on 17 the regression curve compiled for "non-dome" studies at rivers and estuaries by 18 Raymond and Cole (2001). However, their calculation was based on nine observations at wind speeds $< 7 \text{ m s}^{-1}$, whereas all of our observed wind speeds were $> 7 \text{ m s}^{-1}$. Thus, 19 20 the curve in Fig. 5 is extrapolated but is consistent with observed results. 21 Higher values during the low tides are still unidentified, however, following 22 two reasons seems to be possible. First, turbulence caused by bottom friction was 23 enhanced during low tides. The solid curve in Fig. 5 was obtained without observations 24 those had water depth less than 1 m (Raymond and Cole, 2001). In that case, the

1	turbulence created by bottom friction seems to be enhanced. Tokoro et al. (2007; 2008)
2	also showed higher values from Fukido Reef, northern part of Ishigaki Island. They
3	obtained significant difference of $k_{\rm w}$ between the reef and adjacent river mouth and
4	concluded that it was caused by the difference of the bottom roughness. Second, the
5	bubble formation due to wave breaking at the reef crest seems to be also possible. The
6	average of significant wave height during observation periods is 0.6 m, meanwhile the
7	average of water depth at M800 (point at the reef crest) is 0.80 m. Thus, wave breaking
8	and associated bubble-induced gas transfer should occur during low tides. Further
9	investigation is required to clarify the difference of k_w between high and low tides.
10	Finally, contribution of CO_2 gas exchange to the DIC concentration was
11	evaluated. At first, fugacity of CO_2 (f CO_2) in seawater was calculated by the program
12	for CO ₂ system calculation (Lewis and Wallace 1998) using DIC and TA data.
13	Dissociation constants of carbonic acid were derived from the study by Roy et al.
14	(1993). Calculated fCO_2 variation was shown in Fig. 3i, and one can see the variation
15	was almost parallel to that of NDIC (Fig. 3g) due to the relative constancy of NTA to
16	NDIC. It could be also seen that offshore fCO ₂ was almost constant through the
17	observation period, as 367 and 371 μatm for March 7 and 8, respectively. Most of reef
18	water fCO ₂ were above the offshore value except for the daytime of March 8, however
19	seems to be mostly below the atmospheric PCO_2 value of $381\mu atm$, which was monthly
20	average observed at Yonaguni Island 100 km off the Ishigaki Island (Japan
21	Meteorological Agency). Then CO_2 flux over the entire reef was estimated with the
22	average $k_{w,600}$ value of 49 cm h ⁻¹ , atmospheric PCO ₂ of 381 µatm and the solubility
23	provide by Weiss (1974). As shown in Fig. 5b (open diamonds), the entire reef system
24	played a role of absorbing atmospheric CO ₂ during the observation period, however the

1	magnitude of the gas exchange flux was almost 100 times lower than metabolic rates
2	(NCP). If this CO_2 flux was incorporated into the equation 2, final values of k_w would
3	increase 0.2 in average, which was within total error of k_w estimation.
4	
5	CONCLUSIONS
6	We demonstrated gas transfer velocity in a shallow, flowing coral reef
7	environment, using mass balance calculations with two biological tracers. Using
8	nighttime observations, we obtained reasonable gas transfer velocity $k_{\rm w}$ values, all of
9	which exceeded those obtained in wind-dominant studies. The difference is likely due to
10	the contribution of turbulence generated by the interaction of the current and bottom
11	topography.
12	The obtained $k_{\rm w}$ during high tides is consistent with that by Raymond and Cole
13	(2001), whereas k_w during low tides shows higher, which seems to be caused by
14	enhanced friction with the bottom of the reef or bubble-induced gas transfer by wave
15	breaking at the reef crest.
16	
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- 1 Table 1. Calculated $k_{w,600}$, averages of wind speed (U₁₀) and water depth. Wind speeds
- 2 and water depths were averaged values during residence time of reef water. The data
 - $U_{10,avg}$ $(m s^{-1})$ Date and $\begin{array}{c} U_{10,avg} \\ (m \ s^{\text{-1}}) \end{array}$ Tide_{avg} Date and Tide_{avg} kw,600 kw,600 $(cm h^{-1})$ $(cm h^{-1})$ (m) Time (LT) (m) Time Mar 7, Mar 8, 2008 2008 0:00 74 7.4 1.45 0:00 57 8.7 1.66 2:00 36 8.0 1.01 1:00 39 8.3 1.44 4:00 52 8.5 0.74 2:00 37 8.5 1.23 6:00 75 9.4 0.92 3:00 40 1.02 8.6 8:00 50 9.7 1.53 4:00 37 8.8 0.87 30 9.1 68 0.95 9:20 1.76 6:00 8.8 43 9.3 10:00 1.83 7:00 64 9.1 1.18 47 9.1 9:00 165 1.67 11:00 1.80 8.1 127 12:00 -51 8.4 1.62 10:00 8.1 1.80 13:00 -28 7.6 1.39 11:00 -5 7.3 1.81 14:00 -17 7.6 1.12 12:00 -1170 7.5 1.67 15:00 0 8.2 0.84 13:00 -323 7.5 1.40 16:00 18 8.5 0.74 14:00 -403 8.1 1.17 -5 9.2 17:00 0.74 18:00 7 9.2 0.82 19:00 58 9.1 1.07 20.00 45 9.5 1.39 22:00 32 8.7 1.74 23:00 40 8.6 1.74
- 3 during daytime is indicated as italic.

1 Figure legends

2	Figure	1.	Study	site.
2	Figure	1.	Study	site.

3

4	Figure 2. Geographycal map and current trajectories (solid lines with filled circles) of
5	the Kabira Reef. Filled circles represent buoy observation point determined by GPS.
6	Filled stars (M800 and W400) represent points where current meter were situated. At
7	the point E350 inside the reef (filled square), meteorological and oceanographycal
8	observations and water sampling were conducted. Open square located outside the reef
9	represents the point of water sampling for offshore water.
10	
11	Figure 3. Variations of meteorological and oceanographic observations. a) Horizontal
12	wind vectors; b) salinity; c) water depth at sampling point (E350; d) current vectors at
13	the reef crest (M800; d) and sampling point (e); f) saturation degree of dissolved
14	oxygen; g) normalized concentration of dissolved inorganic carbon; h) normalized total
15	alkalinity; i) fugacity of CO ₂ calculated from DIC and TA data. Horizontal lines and
16	filled symbols in g, h and i represent values at offshore, respectively.
17	
18	Figure 4. a) Variation of estimated residence time of reef water (solid line). Filled
19	diamonds represent observation using drifting buoy experiments. Dashed line indicates
20	the variation of average depth of the water trajectory. Error bar (0.06 h) represents the
21	estimated error (5.8% in 1 S. D.) on the average residence time (1.1 h). b) Net
22	community production (NCP) based on the variation of DIC and TA (filled squares) and
23	air-sea CO ₂ flux to the atmosphere (open diamonds). Shaded area represents irradiance.
24	

1	Figure 5. Relationship between transfer velocity normalized to Schmidt number 600 and
2	horizontal wind speed 10 m above sea level. Open triangles and squares represent
3	observed values at low and high tides, respectively. Filled triangle and square represent
4	those averages. The average value during high tide excluded an outlying value during
5	the lowest wind (upper-right). Error bar (4 cm h ⁻¹) represents the estimated relative error
6	(9.3 % in 1 S. D.) on the average value during high tides (43 cm h^{-1}). Solid line
7	represents an regression by Raymond and Cole (2001) based on non-dome observations
8	at estuaries and coasts. Long-dashed line represents the result at Hudson River by
9	Marino and Howarth (1993). Dash-dotted and dotted lines represent wind-dominant
10	schemes studied previously. Small box represents the result by Tokoro et al. (2008) at
11	Fukido Reef (gray triangles) and River (gray squares), Ishigaki Island. Lines in the box
12	represent same regressions as Large box for the horizontal wind speed from 2 to 5 m s ⁻¹ .
13	



2 Figure 1. Study site.



Figure 2. Geographycal map and current trajectories (solid lines with filled circles) of
the Kabira Reef. Filled circles represent buoy observation point determined by GPS.
Stars (M800 and W400) represent points where current meter were situated. At the
point E350 inside the reef, meteorological and oceanographycal observations and water
sampling were conducted. Another square symbol outside the reef represents the point
of water sampling for offshore water.



1	Figure 3. Variations of meteorological and oceanographic observations. a) Horizontal
2	wind vectors; b) salinity; c) water depth at sampling point (E350; d) current vectors at
3	the reef crest (M800; d) and sampling point (e); f) saturation degree of dissolved
4	oxygen; g) normalized concentration of dissolved inorganic carbon; h) normalized total
5	alkalinity; i) fugacity of CO ₂ calculated from DIC and TA data. Horizontal lines and
6	filled symbols in g, h and i represent values at offshore, respectively.



1

2 Figure 4. a) Variation of estimated residence time of reef water (solid line). Filled

3 diamonds represent observation using drifting buoy experiments. Dashed line indicates

4 the variation of average depth of the water trajectory. Error bar (0.06 h) represents the

- 5 estimated error (5.8% in 1 S. D.) on the average residence time (1.1 h). b) Net
- 6 community production (NCP) based on the variation of DIC and TA (filled squares) and
- 7 air-sea CO₂ flux to the atmosphere (open diamonds). Shaded area represents irradiance.



2 Figure 5. Relationship between transfer velocity normalized to Schmidt number 600 and 3 horizontal wind speed 10 m above sea level. Open triangles and squares represent 4 observed values at low and high tides, respectively. Filled triangle and square represent 5 those averages. The average value during high tide excluded an outlying value during 6 the lowest wind (upper-right). Error bar (4 cm h⁻¹) represents the estimated relative error 7 (9.3 % in 1 S. D.) on the average value during high tides $(43 \text{ cm } \text{h}^{-1})$. Solid line 8 represents an regression by Raymond and Cole (2001) based on non-dome observations 9 at estuaries and coasts. Long-dashed line represents the result at Hudson River by 10 Marino and Howarth (1993). Dash-dotted and dotted lines represent wind-dominant 11 schemes studied previously. Small box represents the result by Tokoro et al. (2008) at 12 Fukido Reef (gray triangles) and River (gray squares), Ishigaki Island. Lines in the box 13 represent same regressions as Large box for the horizontal wind speed from 2 to 5 m s⁻¹. 14